

FILE: STRATIF FORTRAN A1 VM/SP HPO REL 4.2 - ELETRONORTE

C DATA SET STRATIFN AT LEVEL 050 AS OF 22/04/86
C DATA SET PEL01230 AT LEVEL 010 AS OF 15/08/85
C

C *****

C THERMAL STRATIFICATION MODEL:

C STRATIF

C (VERSION 2)

C *****

C DEVELOPED BY J.H.G. VERHAGEN EN S. GROOT (VERSION 1),
C MODIFIED BY J.G.C. SMITS (VERSION 2).
C DELFT HYDRAULICS LABORATORY,
C DIVISION OF WATER RESOURCES AND ENVIRONMENT,
C P.O. BOX 177, 2600MH DELFT, THE NETHERLANDS.
C

C *****

C OBJECTIVES:

- C 1. COMPUTATION OF MIXING DEPTH (EXCLUDING ENTRAINMENT IF CHANGE
C OF THE MIXING DEPTH IS INSIGNIFICANT OR NEGATIVE) RESULTING
C FROM EQUALITY OF THE PRODUCTIONS OF POTENTIAL AND KINETIC
C ENERGY IN THE EPILIMNION.
C POTENTIAL ENERGY IS ENLARGED OR REDUCED BY THE NET ENERGY
C FLUX BETWEEN AIR AND WATER AND BY THE INFLOW OF WATER. IT
C IS REDUCED BY ENTRAINMENT AND OUTFLOW OF WATER.
C KINETIC ENERGY IS PRODUCED BY THE WIND AND THE INFLOW.
- C 2. COMPUTATION OF THE AVERAGE TEMPERATURES OF EPILIMNION
C AND HYPOLIMNION (TWO LAYER MODEL).
- C 3. CALCULATION OF THE DISTRIBUTION OF INFLOW AND OUTFLOW
C AMONG EPILIMNION AND HYPOLIMNION. THE MODEL ALLOWS THREE
C INFLOWS FROM DIFFERENT RIVERS, CREEKS OR/AND PRECIPITATION
C AND THREE OUTFLOWS AT DIFFERENT LEVELS.

C *****

C SPECIFICATIONS:

- C 1. THE MAXIMAL NUMBER OF YEARS, WHICH CAN BE SIMULATED IS 20.
C IN CASE CONTINUATION IS DESIRED, CHANGE THE DIMENSIONS
C OF THE ARRAYS.
- C 2. THE TIMESTEP IS A MONTH.

C *****

C INPUT/OUTPUT UNIT NUMBERS:

- C 1 - INPUT OF MODEL PARAMETERS AND OPTIONS
- C 2 - INPUT OF METEOROLOGICAL DATA (TEQ, W, ETC)
- C 3 - INPUT OF HYDROLOGICAL DATA AND INFLOW TEMP. (QI, TI, QO)
- C 4 - OUTPUT TO BE USED AS INPUT FOR OXY

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- C 6 - OUTPUT OF INPUT
- C - OUTPUT OF INTERMEDIATE RESULTS (IF DESIRED)
- C - OUTPUT WITH RESPECT TO THERMAL STRATIFICATION
- C 8 - OUTPUT WITH RESPECT TO HYDROLOGY
- C 9 - OUTPUT WITH RESPECT TO GEOMETRY AND STRATIFICATION

C *****

C ----- DECLARATIONS -----

```

DIMENSION A(2),AT(2),H(2),DH(2),VEPI(2),VHYPO(2),VTOT(2)
DIMENSION CSO(3),HSEL(3),QOS(3)
DIMENSION QIN (20,12),QEIN (20,12),QHIN (20,12),
1 QOUT1(20,12),QOUT2(20,12),QOUT3(20,12),
1 DEPTH(20,12),HEPI (20,12),HYPO (20,12),
1 TEPI (20,12),DELT (20,12),TOUT (20,12),
1 WIND (20,12)
    
```

C ----- DECLARATION OF FORMATS -----

```

101 FORMAT (65X,I1)
102 FORMAT (61X,F5.0)
103 FORMAT (61X,I5)
201 FORMAT (I5,I3,3F8.0)
301 FORMAT (I5,I3,7F7.0)
302 FORMAT (I5,I3,9F7.0)
401 FORMAT (1H , 'AMAX = ',F5.0,1X,'KM2',4X,'GAMMA = ',F5.2,8X,
1 'EXPO = ',F5.2,8X,'RE SL = ',F5.1,1X,'KM',/)
402 FORMAT (1H , 'HZERO = ',F5.1,1X,'M',6X,'HMAX = ',F5.1,1X,'M',6X,
1 'HSEL1 = ',F5.1,1X,'M',6X,'HSEL2 = ',F5.1,1X,'M',6X,
1 'HSEL3 = ',F5.1,1X,'M',/)
403 FORMAT (1H , 'TZERO = ',F5.2,1X,'OC',5X,'DTMP1 = ',F5.2,1X,'OC',5X,
1 'DTMP2 = ',F5.2,1X,'OC',5X,'DTMP3 = ',F5.2,1X,'OC',/)
404 FORMAT (1H , 'CE = ',F5.2,8X,'CVEG = ',F5.2,8X,'CD = ',F5.2,
1 8X,'DISP = ',F5.2,1X,'M2/D',/)
405 FORMAT (1H , 'CP = ',F5.0,1X,'J/KGOC',1X,'RHC = ',F5.0,1X,
1 'KG/M3',2X,'RHQA = ',F5.2,1X,'KG/M3',2X,'BETHA = ',
1 E9.3,/)
406 FORMAT (1H , 'BEGIN = ',I5,8X,'END = ',I5,8X,'DELTT = ',F5.2,
1 1X,'D',6X,'NTS = ',I5,8X,'EPSIL = ',F5.2,1X,'M',/)
407 FORMAT (1H , 'ITITL = ',I5,8X,'INTER = ',I5,8X,'ICUT = ',I5)
502 FORMAT (1H1,10X,22H $$$$ $$$$ $$$$ ,
1 241 $$$ $$$$ $$$ $$$$$,
1 /1X,10X,22H$ $ $ $ ,
1 241$ $ $ $ $ ,
1 /1X,10X,22H $$$$ $ $ $ $ ,
1 241$$$$$ $ $ $$$$ ,
1 /1X,10X,22H $ $ $ $ $ ,
1 241$ $ $ $ $ ,
1 /1X,10X,22H$$$$ $ $ $ $ ,
1 241$ $ $ $ $$$ $ ,//)
503 FORMAT
1 (8X,50H*****
1 8X,50H VERSION 1 JUNE 1984, VERSION 2 APRIL 1986 /
1 8X,50H DELFT HYDRAULICS LABORATORY /
    
```

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1      8X,50H      DIVISION OF WATER RESOURCES AND ENVIRONMENT /
1      8X,50H*****//)
504  FORMAT (1H ,3X,'ECW=',E10.3,3X,'EPA=', E10.3,
1      3X,'EPR=',E10.3,3X,'ECR=',E10.3)
505  FORMAT (1H ,3X,'NIT=',I3,3X,'CE=',F5.1)
601  FORMAT (1H1,'DATE      TE      TH      DELT      TO      TEC      TI1'
1      , '      TI2      TI3      WIND      ETC      DEPTH      DMIX      RVE      RAT'
1      , ' ORLOB'//)
602  FORMAT (1H ,I4,8F6.1,2F6.2,2F6.1,3F6.2)
603  FORMAT (1H ,1X)
605  FORMAT (//,1H , 'ERROR CONCERNING DATES IN INPUT')
801  FORMAT (1H , 'DATE      QIN      QIN1      QIN2      QIN3      QINE',
1      '      QINE1      QINE2      QINE3      QINH      QINH1      QINH2',
1      '      QINH3      QOUT      QOUTE      QOUTH      COEPI',//)
902  FORMAT (1H ,I4,15F8.0,F6.2)
901  FORMAT (1H , 'DATE      DEPTH      HDEPTH      DMIX      AREA      HAREA',
1      '      RAT      VEPI      VHYP0      VTOT      RVE      RVT',
1      '      QVERT      QOUT1      QOUT2      QOUT3',//)
902  FORMAT (1H ,I4,3F8.1,2F8.0,F8.2,3F8.0,2F8.2,4F8.0)
1000  FORMAT ('Q IN ',12F6.0)
1001  FORMAT ('QE IN ',12F6.0)
1002  FORMAT ('QH IN ',12F6.0)
1003  FORMAT ('DEPT ',12F6.1)
1004  FORMAT ('HEP I ',12F6.1)
1005  FORMAT ('HHYP ',12F6.1)
1006  FORMAT ('QOU1 ',12F6.0)
1007  FORMAT ('QOU2 ',12F6.0)
1008  FORMAT ('QOU3 ',12F6.0)
1009  FORMAT ('WIND ',12F6.2)
1010  FORMAT ('TEP I ',12F6.1)
1011  FORMAT ('TDEL ',12F6.1)
1012  FORMAT ('TOUT ',12F6.1)

```

C
C----- READ MODEL AND OPTION PARAMETERS -----
C

```

READ(1,101) ITITLE
READ(1,101) INTER
READ(1,103) IBEGIN
READ(1,103) IEND
READ(1,102) DELTAT
READ(1,103) NTS
READ(1,102) RESL
READ(1,102) HZERO
READ(1,102) TZERO
READ(1,102) HMAX
READ(1,102) AMAX
READ(1,102) EXPO
READ(1,102) GAMMA
READ(1,102) CD
READ(1,102) CVEG
READ(1,102) DTMP1
READ(1,102) DTMP2
READ(1,102) DTMP3
READ(1,102) DISP
READ(1,102) EPSIL

```

```

READ(1,101) IOUT
IF (IOUT .NE. 2) GOTO 5
READ(1,102) HSEL(1)
READ(1,102) HSEL(2)
READ(1,102) HSEL(3)
5 CONTINUE

```

```

C
C-----
C
C HSEL = LEVEL OF OUTLET
C IOUT = OPTION PARAMETER FOR METHOD DISTRIBUTION OF OUTFLOW
C IOUT = 1 : ACCORDING TO RELATIVE EPI LIMNION VOLUME
C IOUT = 2 : ACCORDING TO CRITICAL DISCHARGE (FISHER ET AL)
C

```

C----- ASSIGN VALUES TO PHYSICAL CONSTANTS -----

```

C
BETHA = 0.641E-05
CE = 1.000
CP = 4185.
G = 9.810
RHO = 1000.
RHOA = 1.200

```

C----- WRITE TITLES, INPUT PARAMETERS AND CONSTANTS -----

```

C
IF (ITITLE .NE. 1) GOTO 10
WRITE(6,502)
WRITE(6,503)
10 CONTINUE
WRITE(6,401) AMAX,GAMMA,EXPO,RESL
WRITE(6,402) HZERO,HMAX,HSEL(1),HSEL(2),HSEL(3)
WRITE(6,403) TZERO,DTMP1,DTMP2,DTMP3
WRITE(6,404) CE,CVEG,CD,DISP
WRITE(6,405) CP,RHO,RHOA,BETHA
WRITE(6,406) IBEGIN,IEND,DELTA T,NTS,EPSIL
WRITE(6,407) ITITLE,INTER,IOUT

```

C----- ADJUST UNITIES -----

```

C
DELTA T = DELTA T*86400.
DELTA B = DELTA T/NTS
RESL = RESL*1000.
AMAX = AMAX*(10.**6)
CD = CD/10000.

```

C----- INITIALISATION OF GEOMETRY -----

```

C
H(1) = HZERO
H(2) = H(1)
DH(1) = H(1)
A(1) = AMAX*((1.-GAMMA+(GAMMA*H(1)/HMAX)**EXPO)
AT(1) = A(1)
A(2) = A(1)
AT(2) = AT(1)
VMAX = (1.-(1.-GAMMA)**(EXPO+1.))

```

```

VMAX      = (VMAX*AMAX*HMAX)/(GAMMA*(EXPO+1.))
VTOT(1)   = (1.-GAMMA+(GAMMA*H(1)/HMAX)**(EXPO+1.))
VTOT(1)   = VTOT(1)-(1.-GAMMA)**(EXPO+1.)
VTOT(1)   = (VTOT(1)*AMAX*HMAX)/(GAMMA*(EXPO+1.))
VTOT(2)   = VTOT(1)
VEPI(1)   = VTOT(1)
VEPI(2)   = VEPI(1)
VHYPO(1)  = 0.0
VHYPO(2)  = 0.0
COEPI     = 1.0
    
```

C
 C----- INICIAL HOMOGENECUS TEMPERATURE -----
 C

```

TE = TZERO
TH = TZERO
TO = TZERO
    
```

C
 C-----
 C
 C 1. COMPUTATION OF THE MIXING DEPTH ON THE BASIS OF THE EQUALITY OF
 C KINETIC AND POTENTIAL ENERGY PRODUCTIONS
 C 2. COMPUTATION OF THE TEMPERATURES OF EPILIMNION AND HYPOLIMNION
 C ON THE BASIS OF THE THERMAL ENERGY BALANCE
 C
 C-----

C
 C
 IYEAR = 1
 I = 0
 IP = 2
 12 CONTINUE
 IF (I .EQ. 12) IYEAR = IYEAR+1
 IF (I .EQ. 12) IP = IP +1
 IF (I .EQ. 12) I = 0
 I = I+1
 IF (IYEAR .EQ. 21) GOTO 99

C
 C----- READ THE METEOROLOGICAL DATA, THE INFLOWS, THE TEMPERATURES -----
 C----- OF INFLOW(S) AND THE OUTFLOW(S) -----
 C

```

READ(2,201) LYEAR,LMONTH,TEQ,W,ETC
IF (LYEAR .LT. 1900 .OR. LMONTH .LE. 0 .OR.
1  LMONTH .GT. 12) GOTO 99
READ(3,302) LY,LM,QI1,QI2,QI3,TI1,TI2,TI3,QOS(1),QOS(2),QOS(3)
QQ = QOS(1) + QOS(2) + QOS(3)
QI = QI1 + QI2 + QI3
IF (LYEAR .NE. LY .OR. LMONTH .NE. LM) GOTO 95
LDATE = (LYEAR-1900)*100+LMONTH
    
```

C
 C----- WRITE TITLES FOR OUTPUT -----
 C

```

IF (IP .EQ. 2 .AND. I .EQ. 1) WRITE(6,601)
IF (IP .EQ. 2 .AND. I .EQ. 1) WRITE(8,801)
IF (IP .EQ. 2 .AND. I .EQ. 1) WRITE(9,901)
IF (IP .EQ. 2 .AND. I .EQ. 1) IP = 0
    
```

C

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C----- SYSTEMATICAL ADJUSTMENT OF THE TEMPERATURES OF INFLOWS ----

C
C ALTERNATIVE AS FUNCTION OF DISCHARGE :

C $TI = TB + DT * EXP(-QI/QA)$

C TB = MINIMAL TEMPERATURE

C DT = MAXIMAL INCREMENT OF TEMPERATURE

C QA = THE DISCHARGE FOR WHICH EXP(-1)

C----- ONLY IF DESIRED ----

C $TI1 = TI1 + DTMP1$

C $TI2 = TI2 + DTMP2$

C $TI3 = TI3 + DTMP3$

C----- VOLUME, DEPTH AND AREA AT END OF NEXT MONTH ----

C $VTOT(2) = VTOT(1) + DELTAT * (QI1 + QI2 + QI3 - QO)$

C $H(2) = ((1. - VTOT(2)/VMAX) * ((1. - GAMMA) ** (EXPC + 1.)))$

C $H(2) = H(2) + (VTOT(2)/VMAX)$

C $H(2) = (HMAX/GAMMA) * (H(2) ** (1. / (EXPC + 1.)) - 1. + GAMMA)$

C $A(2) = AMAX * ((1. - GAMMA + (GAMMA * H(2)/HMAX)) ** EXPC)$

C----- DISTRIBUTION INFLOWS AND OUTFLOWS AMONG EPI- AND HYPOLIMNION ----

C IF (TE .NE. TH) GOTO 15

C TX = TH

C IF (TI1 .LT. TH .AND. TI1 .GE. 0.1) TX = TI1

C IF (TI2 .LT. TH .AND. TI2 .GE. 0.1) TX = TI2

C IF (TI3 .LT. TH .AND. TI3 .GE. 0.1) TX = TI3

C IF ((TX-TH) .GT. -1.0) GOTO 15

C TH = TX

C $VHYPO(2) = DELTAT * QI$

15 CONTINUE

C IF (TE .LE. TH) GOTO 100

C TX1 = TI1

C TX2 = TI2

C TX3 = TI3

C IF (TI1 .GE. TE) TX1 = TE

C IF (TI2 .GE. TE) TX2 = TE

C IF (TI3 .GE. TE) TX3 = TE

C IF (TI1 .LE. TH) TX1 = TH

C IF (TI2 .LE. TH) TX2 = TH

C IF (TI3 .LE. TH) TX3 = TH

C $CIEP11 = (TX1 - TH) / (TE - TH)$

C $CIEP12 = (TX2 - TH) / (TE - TH)$

C $CIEP13 = (TX3 - TH) / (TE - TH)$

C GOTO 110

100 CONTINUE

C $CIEP11 = 1.0$

C $CIEP12 = 1.0$

C $CIEP13 = 1.0$

110 CONTINUE

C $QIE1 = CIEP11 * QI1$

```

QIE2 = CIEPI2*QI2
QIE3 = CIEPI3*QI3
QIH1 = QI1-QIE1
QIH2 = QI2-QIE2
QIH3 = QI3-QIE3
QIE = QIE1+QIE2+QIE3
QIH = QI-QIE
    
```

C
C----- DENSITIES FOR POTENTIAL ENERGY -----
C

```

RHTR1 = RHO*(1.-(BETHA*((TI1-4.))**2))
RHTR2 = RHO*(1.-(BETHA*((TI2-4.))**2))
RHTR3 = RHO*(1.-(BETHA*((TI3-4.))**2))
RHTE = RHO*(1.-(BETHA*((TE-4.))**2))
RHTH = RHO*(1.-(BETHA*((TH-4.))**2))
    
```

C
C----- KINETIC ENERGY PRODUCED BY WIND -----
C

```

EKW = ((CD*RHOA)**1.5)*(W**3.75)/(RHO**0.5)
    
```

C
C--- POTENTIAL ENERGY FROM NET FLUX OF ENERGY BETWEEN AIR AND WATER ---
C

```

ALPHA = 2.*BETHA*(TE-4.)
EFLUX = ETC*(TEQ-TE)
EPA = (G*ALPHA*EFLUX)/CP
    
```

C
C----- BEGINNING OF ITERATION FOR COMPUTATION OF MIXING DEPTH -----
C

```

NIT = 0
13 CONTINUE
IF (INTER .EQ. 1) WRITE(6,504) EKW,EPA,EPR,EKR
    
```

C
C----- KINETIC ENERGY PRODUCED BY INFLOW OF RIVER(S) -----
C

```

COHYPO = (1-COEP1)
QTE = (QIE+QO*COEP1)/2
QTH = (QIH+QO*COHYPO)/2
F3 = (A(1)+A(2))/AMAX
F4 = (AT(1)+AT(2))/AMAX
VHE = QTE*F3*RESL/(VEPI(1)+VEPI(2))
IF (VHYPO(1)+VHYPO(2) .LE. 0.00001) GOTO 120
VHH = QTH*F4*RESL/(VHYPO(1)+VHYPO(2))
GOTO 130
120 VHH = 0.0
130 VHORI = ABS(VHE-VHH)
EKR = 0.5*RHO*(VHORI**3.)
    
```

C
C----- POTENTIAL ENERGY PRODUCED BY INFLOW OF RIVER(S) -----
C

```

QOE = COEP1*QO
EPR = ((RHTH-RHTR1)*QIE1 + (RHTH-RHTR2)*QIE2 + (RHTH-RHTR3)*QIE3
1 - (RHTH-RHTE)*QOE)*4.0*G/(A(1)+A(2)+AT(1)+AT(2))
    
```

C
C----- COMPUTE MIXING DEPTH WITHOUT ENTRAINMENT IF CHANGE IS SMALL -----
C----- OR NEGATIVE, BUT CHECK VALUE OF DENOMINATOR -----

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C
D = EPA+EPR
IF (D .LE. 0.) GOTO 17
DH(2) = (EKW+EKR)/(EPA+EPR)
D = DH(2)-DH(1)
IF (D .LE. EPSIL) GOTO 22

```

C----- COMPUTE MIXING DEPTH WITH ENTRAINMENT, BUT CHECK TEMPERATURES -----
C----- SOLUTION IS UNDEFINED IF TE = TH -----

```

17 CONTINUE
IF (TE .LE. TH) DH(2) = H(2)
IF (TE .LE. TH) GOTO 22
DRHO = RHO*BETHA*((TE-4.)**2-(TH-4.)**2)
F1 = CVEG*G*DRHO/DELTAT
F2 = (EPA+EPR-(F1*DH(1)))
DH(2) = ((SQRT((F2**2)+(4.*F1*(EKW+EKR)))-F2)/(F1*2.)

```

C----- TESTS WITH RESPECT TO THE PROGRESS OF THE ITERATION -----
C----- CHOOSE A NEW HYPOLIMNION DEPTH -----

```

22 CONTINUE
IF (DH(2) .GE. H(2)) DH(2) = H(2)
HHO = HH
D = HH-DH(2)
IF (ABS(D) .LE. 0.1) GOTO 26
IF (NIT .GT. 19) DH(2) = (HH+HHO)/2.
IF (NIT .GT. 19) GOTO 26
HH = (HH + DH(2))/2.
IF (NIT .GT. 5 .AND. NIT .LT. 7) HH = (HH + HHO)/2.
IF (NIT .GT. 8 .AND. NIT .LT. 10) HH = (HH + HHO)/2.

```

C----- RECOMPUTE VOLUME, DEPTH AND AREA OF HYPOLIMNION -----

```

HHYPO = AMAX1(0.0, H(2)-HH)
VHYPO(2) = (1.-GAMMA+(GAMMA*HHYPO/HMAX))**(EXPC+1.)
VHYPO(2) = VHYPO(2)-(1.-GAMMA)**(EXPC+1.)
VHYPO(2) = (VHYPO(2)*AMAX*HMAX)/(GAMMA*(EXPC+1.))
VEPI(2) = VTOT(2)-VHYPO(2)
RVE = VEPI(2)/VTOT(2)
AT(2) = AMAX*((1.-GAMMA+(GAMMA*HHYPO/HMAX))**EXPC)

```

C----- COMPUTE DISTRIBUTION OF OUTFLOW(S) -----

```

IF (IOUT .NE. 2) GOTO 25
DO 23 IO = 1,3
HHYPO = H(2)-DH(2)
DLEV = HHYPO-HSEL(IO)
IF (DLEV .LE. 1.) CSO(IO) = 1.
IF (DLEV .LE. 1.) GOTO 23
QCRIT = ((DLEV)**2.5)*(2.-DLEV/HHYPO)*0.1
QCRIT = QOS(IO)/QCRIT
CSO(IO) = 0.
IF (QCRIT .LT. 1.) GOTO 23
CSO(IO) = (2.-DLEV/HHYPO)*0.5

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QCRIT = ALOG10(QCRIT)
QCRIT = (QCRIT)**2.
CSO(IO) = CSO(IO)*(QCRIT+10.62*QCRIT)
CSO(IO) = CSO(IO)/(QCRIT+ 4.88*QCRIT+15.23)
IF (CSO(IO) .GE. 1.) CSO(IO) = 1.

```

```

23 CONTINUE
COEPI = 0.
DO 24 IO = 1,3
IF (QO .GT. 0.) COEPI = COEPI+QOS(IO)*CSO(IO)/QO
24 CONTINUE
25 CONTINUE
IF (IOUT .NE. 2) COEPI = RVE

```

C
C----- RETURN TO BEGINNING OF ITERATION ----
C

```

NIT = NIT+1
GOTO 13
26 CONTINUE
IF (INTER .EQ. 1) WRITE(6,505) NIT,CE

```

C
C----- CHECKS ON THE LOWER AND UPPER LIMITS OF THE MIXING DEPTH ----
C

```

IF (DH(2) .LE. 5. .AND. H(2) .GE. 5.) DH(2) = 5.
IF (DH(2) .GE. H(2)) DH(2) = H(2)

```

C
C----- RECOMPUTE VOLUME, DEPTH AND AREA ----
C

```

HHYPO = H(2)-DH(2)
AT(2) = AMA X*((1.-GAMMA+(GAMMA*HHYPO/HMAX))**EXPO)
VHYPO(2) = (1.-GAMMA+(GAMMA*HHYPO/HMAX))**(EXPC+1.)
VHYPO(2) = VHYPO(2)-(1.-GAMMA)**(EXPC+1.)
VHYPO(2) = (VHYPO(2)*AMAX*HMAX)/(GAMMA*(EXPC+1.))
VEPI(2) = VTOT(2)-VHYPO(2)
RVE = VEPI(2)/VTOT(2)
RVT = VTOT(2)/VMAX
RAT = AT(2)/A(2)

```

C
C----- RECOMPUTE DISTRIBUTION OF OUTFLOW(S) ----
C

```

IF (IOUT .NE. 2) GOTO 29
DO 27 IO = 1,3
HHYPO = H(2)-DH(2)
DLEV = HHYPO-HSEL(IO)
IF (DLEV .LE. 1.) CSO(IO) = 1.
IF (DLEV .LE. 1.) GOTO 27
QCRIT = ((DLEV)**2.5)*(2.-DLEV/HHYPO)*0.1
QCRIT = QOS(IO)/QCRIT
CSO(IO) = 0.
IF (QCRIT .LT. 1.) GOTO 27
CSO(IO) = (2.-DLEV/HHYPO)*0.5
QCRIT = ALOG10(QCRIT)
QCRIT = (QCRIT)**2.
CSO(IO) = CSO(IO)*(QCRIT+10.62*QCRIT)
CSO(IO) = CSO(IO)/(QCRIT+ 4.88*QCRIT+15.23)
IF (CSO(IO) .GE. 1.) CSO(IO) = 1.

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27 CONTINUE
   COEPI = 0.
   DO 28 IO = 1,3
   IF (QO .GT. 0.) COEPI = COEPI+QOS(IO)*CSO(IO)/QO
28 CONTINUE
29 CONTINUE
   IF (IOUT .NE. 2) COEPI = RVE

```

C
C----- COMPUTE OUTFLOWS FROM EPI- AND HYPOLIMNION AND VERTICAL FLOW ---
C----- RESULTING FROM THE CONSERVATION OF MASS ---
C

```

COHYPO = 1.-COEPI
QOE    = COEPI*QO
QOH    = COHYPO*QO
QVERT  = QIE-QOE+(VEPI(1)-VEPI(2))/DELTAT

```

C
C----- IN CASE THE CRITERION OF ORLOB IS EXCEEDED, ---
C----- A HOMOGENEOUS SITUATION OCCURS ---
C

```

RHTEQ = RHO*(1.-(BETHA*((TEQ-4.))**2))
TX = TH
IF (TI1 .LT. TX) TX = TI1
RHTM  = RHO*(1.-(BETHA*((TX-4.))**2))
DGRAV = (RHTM-RHTEQ)/H(2)
IF (DGRAV .GT. 0.0) GOTO 60
ORLOB = 99.
GOTO 65
60 RESL1 = RESL*A(2)/AMAX
HAV     = VTOT(2)/A(2)
ORLOB  = (SQRT(RHO/(G*DGRAV)))*RESL1*(QI+QO)/(2.*HAV*VTOT(2))
IF (ORLOB .LE. 1.) GOTO 30
65 VEPI(2) = VTOT(2)
VHYPO(2) = 0.
DH(2) = H(2)
AT(2) = A(2)
RVE   = 1.
RAT   = 0.
COEPI = 1.
COHYPO = 0.
QOE   = QO
QOH   = 0.
TE    = (TE*VEPI(1) + TH*VHYPO(1))/VTOT(1)
GOTO 32

```

C
C----- COMPUTATION OF TEMPERATURES FROM THE THERMAL ENERGY BALANCE ---
C

```

30 CONTINUE
IF (VHYPO(1) .LE. 0. .AND. VHYPO(2) .LE. 0.) GOTO 33
DVTOT = (VTOT(2)-VTOT(1))/NTS
DVHYPO = (VHYPO(2)-VHYPO(1))/NTS
VEPIO  = VEPI(1)
VHYPO0 = VHYPO(1)
VTOTO  = VTOT(1)
AO     = A(1)
IF (QVERT .LT. 0.) GOTO 32

```

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C
 C----- QVERT => 0, DL/DT < 0 ---
 C

```

DO 75 K=1,NTS
VTOTN = VTOTO + DVTOT
HN     = ((1.-VTOTN/VMAX)*((1.-GAMMA)**(EXPO+1.)))
HN     = HN+(VTOTN/VMAX)
HN     = (HMAX/GAMMA)*(HN**((1.)/(EXPO+1.))-1.+GAMMA)
AN     = AMAX*((1.-GAMMA+(GAMMA*HN/HMAX))**EXPC)
VHYPO = VHYPOD + DVHYPO
VEPIN  = VTOTN - VHYPON
F5     = (ETC*(AO+AN))/(2.*RHO*CP)
F8     = QIE1*TI1+QIE2*TI2+QIE3*TI3
F6     = (VEPIO+VEPIN)/(2.*DELTB)
TEN    = (F6*TE+F5*(TEQ-TE/2.))+F8-QIE*TE/2./
1      (F6+F5/2.+QIE/2.)
F8     = QIH1*TI1+QIH2*TI2+QIH3*TI3
F6     = (VHYPOD+VHYPON)/(2.*DELTB)
TH     = (F6*TH+F8-QIH*TH/2.+QVERT*(TEN+TE-TH)/2.)/
1      (F6+QIH/2.+QVERT/2.)
TE     = TEN
VTOTO  = VTOTN
AO     = AN
VHYPOD = VHYPON
VEPIO  = VEPIN
75 CONTINUE
GO TO 34
    
```

C
 C----- QVERT < 0, DL/DT > 0 ---
 C

```

32 CONTINUE
DO 76 K=1,NTS
VTOTN = VTOTO + DVTOT
HN     = ((1.-VTOTN/VMAX)*((1.-GAMMA)**(EXPO+1.)))
HN     = HN+(VTOTN/VMAX)
HN     = (HMAX/GAMMA)*(HN**((1.)/(EXPO+1.))-1.+GAMMA)
AN     = AMAX*((1.-GAMMA+(GAMMA*HN/HMAX))**EXPC)
VHYPO = VHYPOD + DVHYPO
VEPIN  = VTOTN - VHYPON
F5     = (ETC*(AO+AN))/(2.*RHO*CP)
F8     = QIH1*TI1+QIH2*TI2+QIH3*TI3
F6     = (VHYPOD+VHYPON)/(2.*DELTB)
THN    = (F6*TH+F8-QIH*TH/2.)/
1      (F6+QIH/2.)
F8     = QIE1*TI1+QIE2*TI2+QIE3*TI3
F6     = (VEPIO+VEPIN)/(2.*DELTB)
TE     = (F6*TE+F5*(TEQ-TE/2.))+F8-QIE*TE/2.+QVERT*(TE-THN-TH)/2./
1      (F6+F5/2.+QIE/2.-QVERT/2.)
TH     = THN
VTOTO  = VTOTN
AO     = AN
VHYPOD = VHYPON
VEPIO  = VEPIN
76 CONTINUE
GO TO 34
    
```

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C
 C-----HOMOGENECUS SITUATION-----
 C

```

33 CONTINUE
QIE1 = QI1
QIE2 = QI2
QIE3 = QI3
QIE = QI
QIH1 = 0.0
QIH2 = 0.0
QIH3 = 0.0
QIH = 0.0
QVERT = QIE-QOE+(VEPI(1)-VEPI(2))/DELTAT
DVTOT = (VTOT(2)-VTOT(1))/NTS
VEPIO = VEPI(1)
VTOTO = VTOT(1)
AO = A(1)
DO 77 K=1,NTS
VTOTN = VTOTO + DVTOT
HN = ((1.-VTOTN/VMAX)*(1.-GAMMA)**(EXPO+1.))
HN = HN+(VTOTN/VMAX)
HN = (HMAX/GAMMA)*(HN**(1./(EXPO+1.))-1.+GAMMA)
AN = AMAX*((1.-GAMMA+(GAMMA*HN/HMAX))**EXPO)
VEPIN = VTOTN
F5 = (ETC*(AO+AN))/(2.*RHO*CP)
F8 = QIE1*TI1+QIE2*TI2+QIE3*TI3
F6 = (VEPIO+VEPIN)/(2.*DELTB)
TE = (F6*TE+F5*(TEQ-TE/2.)+F8-QIE*TE/2.)/
1 (F6+F5/2.+QIE/2.)
VTOTO = VTOTN
AO = AN
VEPIO = VEPIN
77 CONTINUE
    
```

C
 C-----SOME FINAL CHECKS AND CALC. OF OUTFLOW TEMPERATURE-----
 C

```

34 CONTINUE
IF (VHYPO(2) .LE. 0.) TH = TE
TO = COEPI*TE+COHYPO*TH
35 CONTINUE
IF (TE .EQ. TH) GOTO 37
IF (TE .GT. TH) GOTO 36
TE = (VEPI(2)*TE+VHYPO(2)*TH)/VTOT(2)
TH = TE
TO = TE
VHYPO(2) = 0.
VEPI(2) = VTOT(2)
DH(2) = H(2)
RVE = 1.
GOTO 37
36 CONTINUE
    
```

C
 C-----BALANCE INCLUDING VERTICAL DISPERSION-----
 C

```

IF (DISP .LT. 0.01) GOTO 37
    
```

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```

F7 = DISP*(TE-TH)/(0.5*H(2))
TE1 = TE-(F7*(AT(1)+AT(2))*DELTA T)/((VEPI(1)+VEPI(2))*86400.)
TH1 = TH+(F7*(AT(1)+AT(2))*DELTA T)/((VHYPO(1)+VHYPO(2))*86400.)
IF (TE1 .GT. TH1) TE = TE1
IF (TH1 .GT. TH) TH = TH1
IF (TE1 .GT. TH1) GOTO 37
TE = (VEPI(2)*TE+VHYPO(2)*TH)/VTOT(2)
TH = TE
TO = TE
VHYPO(2) = 0.
VEPI(2) = VTOT(2)
DH(2) = H(2)
COEPI = 1.
RVE = 1.
RAT = 0.

```

C
C----- INITIALISATION OF THE NEXT MONTH -----
C

```

37 CONTINUE
DH(1) = DH(2)
H(1) = H(2)
A(1) = A(2)
AT(1) = AT(2)
VTOT(1) = VTOT(2)
VEPI(1) = VEPI(2)
VHYPO(1) = VHYPO(2)

```

C
C----- PREPARATION OF OUTPUT FOR OXY -----
C

```

IF (ORLOB .GE. 99.) ORLOB = 99.
DEPTH(IYEAR,I) = H(2)
HYPO (IYEAR,I) = H(2)-DH(2)
HEPI (IYEAR,I) = DH(2)
TEPI (IYEAR,I) = TE
DELT (IYEAR,I) = TE-TH
TOUT (IYEAR,I) = TO
QIN (IYEAR,I) = QI
QEIN (IYEAR,I) = QIE
QHIN (IYEAR,I) = QIH
QOUT1(IYEAR,I) = QOS(1)
QOUT2(IYEAR,I) = QOS(2)
QOUT3(IYEAR,I) = QOS(3)
WIND (IYEAR,I) = W
HHYPO2 = H(2)-DH(2)
DLT = TE-TH
A2 = A(2)/(10.0**6)
AT2 = AT(2)/(10.0**6)
VEPI2 = VEPI(2)/(10.0**6)
VHYPO2 = VHYPO(2)/(10.0**6)
VTOT2 = VTOT(2)/(10.0**6)

```

C
C----- WRITE OUTPUT -----
C

```

WRITE(6,602) LDATE,TE,TH,DLT,TO,TEQ,TI1,TI2,TI3,W,ETC,H(2),

```

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```

1          DH(2),RVE,RAT,ORLOB
  IF (I .EQ. 12) WRITE(6,603)
  WRITE(8,802) LDATE,QI,QI1,QI2,QI3,QIE,QIE1,QIE2,QIE3,QIH,QIH1,
1          QIH2,QIH3,QO,QOE,QOH,COEPI
  IF (I .EQ. 12) WRITE(8,603)
  WRITE(9,902) LDATE,H(2),HHYP02,DH(2),A2,AT2,RAT,VEPI2,VHYPO2,
1          VTOT2,RVE,RVT,QVERT,QOS(1),QOS(2),QOS(3)
  IF (I .EQ. 12) WRITE(9,603)

```

```

C
C----- START A NEW COMPUTATION FOR THE NEXT MONTH ----
C

```

```

  GO TO 12
99 CONTINUE

```

```

C
C----- WRITE THE INPUT FOR OXY ----
C

```

```

  IYEAR = IYEAR-1
  DO 50 I=1,IYEAR,2
  WRITE(4,1000) (QIN(I,J),J=1,12)
  WRITE(4,1000) (QIN(I+1,J),J=1,12)
  WRITE(4,1001) (QEIN(I,J),J=1,12)
  WRITE(4,1001) (QEIN(I+1,J),J=1,12)
  WRITE(4,1002) (QHIN(I,J),J=1,12)
  WRITE(4,1002) (QHIN(I+1,J),J=1,12)
  WRITE(4,1003) (DEPTH(I,J),J=1,12)
  WRITE(4,1003) (DEPTH(I+1,J),J=1,12)
  WRITE(4,1004) (HEPI(I,J),J=1,12)
  WRITE(4,1004) (HEPI(I+1,J),J=1,12)
  WRITE(4,1005) (HYPO(I,J),J=1,12)
  WRITE(4,1005) (HYPO(I+1,J),J=1,12)
  WRITE(4,1006) (QOUT1(I,J),J=1,12)
  WRITE(4,1006) (QOUT1(I+1,J),J=1,12)
  WRITE(4,1007) (QOUT2(I,J),J=1,12)
  WRITE(4,1007) (QOUT2(I+1,J),J=1,12)
  WRITE(4,1008) (QOUT3(I,J),J=1,12)
  WRITE(4,1008) (QOUT3(I+1,J),J=1,12)
  WRITE(4,1009) (WIND(I,J),J=1,12)
  WRITE(4,1009) (WIND(I+1,J),J=1,12)
  WRITE(4,1010) (TEPI(I,J),J=1,12)
  WRITE(4,1010) (TEPI(I+1,J),J=1,12)
  WRITE(4,1011) (DELT(I,J),J=1,12)
  WRITE(4,1011) (DELT(I+1,J),J=1,12)
  WRITE(4,1012) (TOUT(I,J),J=1,12)
  WRITE(4,1012) (TOUT(I+1,J),J=1,12)

```

```

50 CONTINUE

```

```

C
C----- END OF STRATIF ----
C

```

```

  GO TO 96
95 WRITE(6,605)
96 CONTINUE
  STOP
  END

```